THE SPRING RESEARCH AND MANUFACTURERS' ASSOCIATION

COMPARISON OF BRITISH AND FOREIGN STANDARD SPECIFICATIONS FOR SPRING MATERIALS

Report No. 418

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Report No 418

CON	DENIS	Page No
1.	INTRODUCTION	1
2.	COLD DRAWN CARBON STEEL SPRING WIRE	3
3.	MUSIC STEEL SPRING WIRE	10
4.	PRE-HARDENED AND TEMPERED CARBON STEEL SPRING WIRE	14
5.	1% CHROME-VANADIUM OIL HARDENED AND TEMPERED SPRING WIRE	20
6.	SILICON-CHROME PRE-HARDENED AND TEMPERED SPRING WIRE	24
7.	STAINLESS STEEL SPRING WIRE	28
8.	MOLYBDENUM-BEARING STAINLESS STEEL SPRING WIRE	32
9.	17/7 PH STAINLESS STEEL SPRING WIRE	36
10.	SPRING BRASS AND COPPER-NICKEL SPRING WIRE	40
11.	PHOSPHOR BRONZE SPRING WIRE	44
12	COPPER-REDYLLTIM SPRING WIRE	47

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1. INTRODUCTION

This report collects together the articles presented in a monthly series in SRAMA's Newsletter, tabulating British and equivalent foreign standards for an exhaustive range of materials for wire springs.

The series appeared in the Technical section of the Newsletter between September 1986 and July 1987 and covered eleven material qualities whose major features, for ease of reference, were presented in tabular form for composition, tensile strength, formability and surface quality.

wherever possible, to facilitate production of the report, the original text and format have been reproduced, which explains the lack of consistency in type-face and size (especially in the tables, some of which had to be reduced to fit the physical constraints of paper size). However, every effort has been made to excise repetitions and irrelevancies.

We hope that members will find this of value as a reference document, to be used as an extension of the information contained in SRAMA's "Spring Materials Selector".

Explanatory Notes:-

(a) The major features of the various national specifications listed should be sufficient for most purposes. For more detailed comparison, the up-to-date editions of the standards quoted should always be consulted since similar specifications do vary in minor details.

(b) Many spring users indicate their requirements by reference only to material composition rather than specifying the appropriate spring wire standard. Attention is drawn to the fact that the use of 'steel grade' numbers defines only the chemical composition and not the mechanical and metallurgical conditions.

2. COLD DRAWN CARBON STEEL SPRING WIRE

Carbon steel spring wire is by far the most important and widely used material for the manufacture of light helical springs. It derives its strength from a combination of heat treatment (Patenting) and cold working by drawing. These wires are produced to a variety of quality grades by rod selection, composition and the degree of control exercised on surface imperfections.

A. COMPOSITION

Wire Specification	Origin	Steel Grade	% C	% Si	% Mn	% S max	% P max	
BS 5216 1975	UK	NS HS ND	0.45- 0.85 0.45- 0.85 0.55- 0.85	0.35 max 0.35 max 0.35 max 0.35 max	0.4- 1.0 0.4- 1.0 0.3- 1.0	0.05 0.05 0.03 0.03	0.05 0.05 0.03	
S201:1967 S202:1967	UK		0.85 0.55- 0.85 0.55- 0.85	0.1- 0.35 0.1- 0.35	1.0 0.3- 1.0 0.3- 1.0	0.03	0.03	
DEF106:1961	UK		0.75- 0.85	0.3 max	0.5- 0.7	0.02	0.02	
ASTM A227 1983	US		0.45- 0.85	0.15~ 0.35	0.3- 1.3	0.05	0.04	
ASTM A679 1983	us		0.65- 1.0	0.1- 0.4	0.2- 1.3	.0.05	0.04	
SAE J113:69	US	1 2	0.45- 0.75 0.50- 0.85	0.1- 0.3 0.1- 0.3	0.6- 1.3 0.6- 1.3	0.05	0.04	
SAE J271:72	US		0.7- 1.0	0.1- 0.3	0.2- 1.3	0.04	0.04	
SAE J172:70	US		0.6- 0.75	0.15- 0.3	0.6- 0.9	0.03	0.025	
DIN 17223 Part 1:1984	Germany	A B*	0.4- 0.85 0.4- 0.85	0.35 max	0.3- 1.0 0.3- 1.5	0.04	0.04	Cu 0.2
SIS 141774: 1979	Sweden	1774- 04 1774- 05	0.6- 0.95 0.6- 0.95	0.15- 0.4 0.15- 0.4	0.3- 0.8 0.3- 0.8	0.035	0.035	
G 3521:1980	Japan	SW-A SW-B SW-C	0.39- 0.86	0.15- 0.35	0.3-	0.04	0.04	

* The German DIN 17223 steel grade B specifies three carbon and manganese ranges within those quoted in the table to accommodate increases in section size.

Commentary:

The Japanese standard G3521 does not specify compositions but refers to G3506 which contains a series of 21 steels having more closely defined carbon contents, each of 0.07% range. The choice of carbon level is governed by the tensile strengths specified in G3521, the selection being made by the manufacturer.

The majority of the standards specify fairly wide carbon ranges but, in practice, wire manufacturers will select a somewhat tighter range depending on the type of patenting employed, the finished wire size and the required tensile strength.

B. TENSILE STRENGTH

	2 Strength Rm (N/mm)							
Wire Dia (mm)	Grade l (NS)	BS 5216 Grade 2 (NS,HS,ND,HD)	Grade 3 (HS,ND,HD)	S201	S202			
0.10 0.20 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.0 15.0 20.0	1370-1570 1250-1450 1170-1370 1110-1310 1050-1250 1010-1210 970-1170 940-1140	2340-2640 2060-2320 1790-2010 1570-1770 1450-1650 1370-1570 1310-1510 1250-1450 1210-1410 1170-1370 1140-1340 1120-1320 1060-1260	2640-2940 2320-2580 2010-2230 1770-1970 1650-1850 1570-1770 1510-1710 1450-1650 1410-1610 1370-1570 1340-1540 1320-1520 1260-1460	2317 min 2162 min 1853-2008 1699-1853 1544-1699 1390-1544 1390-1544 1235-1390 1081-1235 1081-1235 1081-1235	2471 min 2317 min 2008-2162 1853-2008 1699-1853 1544-1699 1544-1699 1390-1544 1235-1390 1235-1390 1235-1390 1235-1390			

	2 Strength Rm (N/mm)							
Wire Dia (mm)	DEF 106	AS Class I	TM A227 Class II	ASTM A679	SAE Class l	J113 Class 2		
0.10 0.20 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.0 15.0 20.0	2625 min 2625 min 2239-2394 2008-2162 1776-1930 1621-1776 1621-1776 1544-1699 1467-1622	1960-2240 1770-2040 1580-1810 1460-1680 1380-1590 1320-1510 1280-1470 1220-1410 1190-1370 1160-1340 1130-1310 1090-1260 1030-1190	2240-2520 2040-2310 1810-2040 1680-1900 1600-1900 1510-1700 1470-1650 1410-1600 1370-1550	2410-2670 2160-2390 1940-2150 1810-2000 1730-1910 1650-1830	1960-2240 1770-2040 1580-1810 1460-1680 1380-1590 1320-1510 1280-1470 1220-1410 1200-1380 1160-1340 1140-1320 1100-1270	2240-2520 2040-2310 1810-2040 1680-1900 1600-1900 1510-1700 1470-1650 1410-1600 1380-1560 1340-1530 1320-1510 1270-1450		

	Strength Rm (N/mm)							
Wire Dia (mm)	SAE J271	SAE J172	DIN 1722 Grade A	3: Part l Grade B	SIS 1 1774-04	4 17 74 1774-05		
0.10 0.20 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.0 15.0 20.0	2415-2670 2165-2400 1945-2150 1815-2005 1730-1910 1650-1830 1600-1775 1545-1720 1500-1675 1470-1650 1440-1610 1380-1550	1620-1758 1620-1758 1586-1724 1517-1655 1482-1620	1720-1970 1520-1750 1410-1620 1320-1520 1260-1450 1210-1390 1160-1340 1120-1300 1090-1260 1060-1230	2200-2470 1980-2220 1760-1970 1630-1830 1530-1730 1460-1650 1400-1580 1350-1530 1310-1480 1270-1440 1240-1400 1180-1340 1110-1260 1020-1150	1900-2200 1750-2000 1550-1800 1500-1750 1400-1650 1300-1500 1200-1400 1200-1400 1150-1350 1150-1350 1050-1250	2750-3100 2650-3000 2450-2750 2300-2550 2050-2250 1850-2050 1750-1950 1650-1850 1500-1700 1400-1600 1400-1600 1350-1550 1350-1550 1250-1450		

	1						
:	Strength Rm (N/mm ²) J.I.S G352l						
Wire Dia (mm)	Class A	Class B	Class C				
0.10	2010-2350	2350-2700	2700-3040				
0.20 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.0 15.0 20.0	1910-2210 1620-1910 1470-1720 1270-1470 1180-1370 1180-1370 1130-1320 1030-1230 980-1180 980-1180 930-1130 930-1130	2210-2500 1910-2210 1720-1960 1470-1720 1370-1570 1320-1570 1320-1520 1230-1420 1180-1370 1180-1370 1130-1320 1130-1320 1080-1280	2500-2800 2210-2500 1960-2210 1720-1960 1570-1810 1570-1770 1520-1720 1420-1620 1370-1570 1370-1570 1320-1520 1320-1520 1280-1470				

- Notes:- i) The UK defence standard DEF 106 specifies a reduction of area on tensile testing of greater than 35% for all wires above 1.2 mm diameter.
 - ii) The SAE J172 standard calls for 40% minimum R of A on all sizes.
 - iii) The German DIN 17223 specifies minimum reduction of areas as:1 mm to less than 4 mm wires 40%; 4 mm to 7 mm wires 35%; 7 mm to 10 mm sizes, 30%.

Commentary:

All countries offer more than one tensile range to cater for springs that are lowly stressed as well as for those where the operating stresses are high. In addition, the UK and Japan provide an extra class of material where the tensile strengths are relatively low to satisfy applications where material of high formability is needed. On the whole, the highest tensile

strengths are obtained from BS 5216 Grade 3, and the American standards A679 and J271.

The new German and ASTM standards now extend their sizes beyond $12\,$ mm diameter and, in the case of the former, this is increased to $20\,$ mm.

C. FORMABILITY

			 	T
Specification	Torsion Test (mm)	Bend Test (180 ⁰)	Wrap Test (mm)	Wrap and Stretch Test (mm)
BS 5216 all	>.4 to 10	3 to 6.5	<3 on ld	
qualities		on 2d >6.5 on 3d		
S201	<5.1	>2.2*	<2.2	
S202 DEF 106	<5.1 all sizes	>2.2*	<2.2 .5 to 2	
A227 Class I			on 2d .5 to 2	
7			on 2 d >4 to 8 on 2d	
A227 Class II			.5 to 4	
п			on 2d >4 to 8 on 4d	
A679			.5 to 3	
			on 2d >3 to 5.2 on 4d	
J113			as A227	
J271			.5 to 4	
			on 2d >4 to 7.9 on 4d	
J172				
DIN 17223	>.7 to 7			<.7 on 3d
Grades A and B	>7 to 10 Guidance only			(Grade B only)
SIS 1774-04	.5 to 5	>5 on 4d	<2.5 on 1d	
and -05 G3521	<6	>6*	<6 on ld	

^{*}S201, S202 and G3521 are subject to a 90° reverse bend test.

Commentary:

The majority of standards favour the wrap test as a means of assessing formability. None of the American standards uses the torsion test or the bend test as a method of determining formability, the SAE valve spring wire standard J172 having no requirements at all with respect to assessing formability.

D. SURFACE QUALITY

Specification	Deep Etch Test	Max Defect depth	Complete	Decarbur: Partial	isation Gradient	Total
BS 5216 NS	all sizes					
HS ND HD S201	all sizes all sizes all sizes all sizes	3% 1.5% Nil	Nil Nil Nil Nil	3% 1.5% Nil 1.5%	Nil	3% 1.5% Nil 1.5%
S202 DEF 106	all sizes all sizes	Nil Nil	Nil Nil	Nil Nil	Nil Nil	Nil Nil
A227		*				
A679 J113		* 3.5% or				
J271 J172	all sizes	0.25 mm whichever is smaller "	Nil	0.025 to 0.037 mm depending		
DIN 17223		*		on size		
Grades A & B SIS 1774-04		*				
and -05 G3521		*				

^{*} only general statements that wire shall be free from harmful defects.

Commentary:

It is clear that the UK places more importance on the deep etch test than its foreign counterparts. It is also significant that few of the foreign standards quantify maximum allowable defect depths and, of the foreign standards examined, only J172 (a valve spring quality) places any restriction on surface decarburisation. When making this comparison, however, it should be noted that the high quality Grades C and D of DIN 17223 have not been included here since they are essentially music wire and are considered in Chapter 3 of this report.

3. MUSIC STEEL SPRING WIRE

Music steel spring wire is produced from steel having a higher carbon content than the general purpose patented cold drawn spring wires. It is characterised by its very high tensile strength and high surface quality and is particularly suitable for spring and wire form applications subjected to high stresses.

A. COMPOSITION

Wire Specification	Origin	Steel Grade	%C min max	%Si min max	%Mn min max	%S max	%P max
BS5216 1975	UK	М	0.70-1.00	0.35	0.25-0.75	0.03	0.03
ASTM A228:83	US		0.70-1.00	0.10-0.30	0.20-0.60	0.03	0.025
SAE J178:70	US		0.80-1.00	0.10-0.30	0.20-0.60	0.03	0.025
DIN 17223 Sheet 1:84	Germany	C and D	0.50-1.00	0.35	0.30-1.50	0.03	0.03
SIS 14-17-74:79	Sweden	17 74-06	0.60-0.95	0.15-0.40	0.30-0.80	0.035	0.035
JIS G3522:82	Japan	SWP - A SWP - B SWP - V	0.60-0.95 0.60-0.95 0.60-0.95	0.12-0.32 0.12-0.32 0.12-0.32	0.30-0.60 0.60-0.90 0.30-0.90	0.025 0.025 0.025	0.025 0.025 0.025

Note:- The copper content of wires to G3522 is specified as 0.20% max. for SWP-A and SWP-B wires. The valve spring wire SWP-V has a limiting value for copper of 0.15%. The standard G3522 does not specify the actual composition of wires but refers the reader to G3502 which includes a series of 18 steels having more closely defined carbon contents, each of 0.05% range.

Commentary:

The UK and US standards in general specify higher minimum carbon contents than do the German, Swedish and Japanese standards.

B. TENSILE STRENGTH

		Strength Rm (N/mm ²)									
Wire Dia (mm)	BS52 Grade 4	216 M Grade.5	A228 and J178	DIN] Grade C	17223 Grade D	SIS 1774 <i>-</i> 06					
0.10 0.20 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0 12.5 16.0 20.0	3020-3400 2760-3090 2440-2670 2240-2390 1970-2120 1850-2000 1770-1920	3400-3780 3090-3420 2670-2900 2390-2540 2120-2270 2000-2150	3000-3300 2700-3000 2400-2650 2150-2400 1950-2200 1800-2000 1700-1900 1650-1850 1660-1800	1980-2200 1840-2040 1740-1930 1660-1840 1590-1770 1540-1710 1490-1660 1450-1610 1410-1570 1330-1480 1240-1390 1160-1300	2800-3100 2800-3100 2480-2740 2230-2470 1980-2200 1840-2040 1740-1930 1660-1840 1590-1770 1540-1710 1490-1660 1450-1610 1410-1570 1330-1480 1240-1390 1160-1300	3150-3500 2900-3200 2650-2900 2400-2650 2150-2350					

	Strength Rm (N/mm ²)					
Wire Dia (mm)	G3522 SWP-A	G3522 SWP-B	G3522 SWP-V			
0.10 0.20 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0	2795-3089 2599-2844 2305-2550 2059-2256 1814-2010 1667-1863 1667-1814 1618-1765 1520-1667 1471-1618 1471-1618 1422-1569	3089-3383 2844-3089 2550-2795 2256-2452 2010-2206 1863-2059 1814-1961 1765-1912 1667-1814	1765-1912 1667-1814 1667-1814 1618-1765 1520-1667			

Note:- The German DIN 17223 Sheet 1 standard specifies minimum reduction of area values as 1 mm to 3.8 mm wires 40%; 4 mm to 7 mm wires, 35%; 7.5 mm to 10 mm wires, 30%.

Commentary:

The British Grade 5 music wire has, in general, the highest tensile strength when compared with foreign standards for similar sized wires. Historically, music wires have been confined to sizes less than about 4 to 6 mm but both the Germans and Japanese have recently introduced 'music or piano' wires which extend to 20 mm diameter and 10 mm diameter respectively.

C. FORMABILITY

Specification	Torsion Test	Bend Test (90 ⁰)	Wrap Test	Wrap & Stretch Test
BS5216 M			>0.2mm on	
A228 and J178			all sizes on 1d (J178 only)	<2.6mm on 3d extend to 3 times length
DIN 17223 Sheet 1	O.7 to 7mm >7 to lOmm guidance only		<u></u>	<0.7mm on 3d extend to 2 to 4 times the coiled length
SIS 17 74-06	0.5 to 5mm	>5mm (180°)	<2.5mm on ld	
G3522	<6mm	>6mm		guidance only

Commentary:

Comparing the above standards, there would appear to be little common ground with respect to a preferred formability test. Clearly the bend test is least popular but, for small wire sizes, foreign standards seem to favour a wrap and stretch test.

D. SURFACE QUALITY

Specification	Deep Etch test	Max defect depth	Complete	Decarburis Partial	ation Gradient	Total
BS5216 M	all sizes	1.5%	Nil	1.5% Max		
A228						
J178	all sizes	1%		1% Max		
DIN 17223. Grade D	all sizes	1%	Nil	1.5% Max		
SIS 17 74-06						
G3522 SWP-A SWP-B	>1.Omm	0.02 to 0.08mm according to wire size				
SWP-V	>1.Omm	0.01 to 0.03mm according to wire size	Nil			1.5% or 0.05mm Max

Commentary:

All standards (with the exception of A228) stipulate deep etch testing and specify maximum defect levels as a percentage of wire diameter or, in the case of the Japanese standard, as a dimension. For the SWP-A and SWP-B qualities, these dimensions equate to approximately 1% of the wire diameter. For the SWP-V wire, maximum defect levels equate to 0.5% of the wire diameter.

Limits on decarburisation at 1 to 1.5% are similar and none of the standards allows complete decarburisation. It is surprising, however, that the American A228 and Japanese G3522, SWP-A and B qualities do not specify limits on decarburisation.

4. PRE-HARDENED AND TEMPERED CARBON STEEL SPRING WIRE

A. COMPOSITION

Wire Specification	Origin	Steel Grade	%C Min Max	%Si Min Max	%Mn Min Max	%S Max	%P Max
BS 2803 1980	UK	095A65 094A65 093A65	0.55 0.75 0.55 0.75 0.55 0.75	0.30 0.30 0.30	0.60 1.20 0.60 1.20 0.60 1.20	0.05 0.04 0.03	0.05 0.04 0.03
ASTM A229: 83	US	-	0.55 0.85	0.15 0.35	0.30 1.20	0.05	0.04
ASTM A230: 83	US	-	0.60 0.75	0.15 0.35	0.60 0.90	0.03	0.025
SAE J316: 70 SAE J351: 68	us us	А В ~	0.60 0.85 0.60 0.75 0.60-0.75	0.15 0.30 0.15-0.30 0.15 0.30	0.90 1.20 0.60 0.90 0.60 0.90	0.05 0.05 0.03	0.04 0.04 0.025
DIN 17223 Sheet 2: 64	Germany	FD VD	0.60-0.70	0.25 0.25	0.50 0.90 0.50 0.90	0.03 0.02	0.03 0.03
SIS 14-17-70; 85	Sweden	1770-03	0.65-0.80	0.15-0.40	0.50 0.80	0.035	0.035
G3560: 83 -G3561: 82	Japan Japan	SWO-A SWO-B SWO-V	0.54-0.76 0.64-0.86	0.15-0.35 0.15-0.35	0.30-0.90 0.30-0.90	0.04 0.03	0.04 0.03

Note: The compositions given for G3560 and G3561 encompass a series of carbon steels whose carbon, manganese, sulphur and phosphorous contents are more closely defined.

Commentary:

All the steels have carbon contents around the eutectoid composition, with the German steels having the narrowest range of carbon. As would be expected, the higher valve spring wires limit the sulphur and phosphorus contents to lower levels. All qualities contain appreciable amounts of manganese to aid hardenability and, in the case of SAE J316, quote two manganese ranges depending on the final size of wire to be heat treated. For example, for wire sizes greater than 4.8mm, the high manganese range of 0.9 to 1.2% is specified.

B. TENSILE STRENGTH

(See overleaf)

Note: Specifications A230, J351, DIN 17223 FD and VD, and G3561 specify a minimum reduction of area of the tensile test piece, eg A230, J351 wires over 2.5mm diameter - 40% minimum; DIN 17223 FD and VD wires, a variable minimum R of A value ranging from 35% to 45% according to wire size: G3561 wires, < 4 mm 45% min, > 4 mm 40% min.

Commentary:

Comparing the 13 different pre-hardened and tempered tensile ranges, only the American ASTM and SAE specifications have identical tensile properties. Because of the variation in tensile properties among the other standards, care is needed when attempting to equate one wire standard with another. In general, the UK and German FD quality wires appear to have the nearest similarity regarding tensile strength. There would seem to be no consistent pattern with respect to the tensile strengths of valve spring quality wires when compared with their own national general purpose standards.

B. TENSILE STRENGTH (PRE-HARDENED AND TEMPERED CARBON STEEL)

Wire Dia (mm)					Strength Rm (N/mm ²)	(N/mm ²)				
	BS 2803	A229 Cless I and J316 Class I	A229 Class II and J316 Class II	A230 and J351	DIN 17223 FD	DIN 17223 VD	SIS 1770-03	63560 SW0-A	G3560 SWO-B	G3561 SWD-V
0.25 1.0 2.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 10.0 12.5 14.0	1910-2170 1860-2110 1770-2000 1630-1800 1540-1690 1480-1630 1430-1580 1360-1530 1350-1500 1370-1470 1300-1450 1240-1430	2050-2250 1800-2000 1600-1800 1500-1700 1400-1580 1350-1520 1300-1480 1280-1450 1280-1450 1220-1400 1200-1300 1120-1300	2230-2450 2060-2280 1820-2020 1690-1860 1600-1780 1520-1700 1480-1660 1450-1630 1430-1630 1400-1580 1350-1530 1320-1500	1700-1850 1650-1800 1600-1750 1580-1720 1520-1680 1500-1650	1765-1961 1618-1765 1520-1667 1400-1628 1402-1550 1402-1550 1363-1510 1295-1442 1295-1442 1295-1402 1255-1402	1667-1814 1520-1618 1432-1530 1402-1500 1344-1442 1304-1402	1600-1800 1550-1750 1500-1700 1450-1600 1400-1550 1350-1500 1300-1450 1300-1450	1569-1716 1471-1618 1422-1569 1373-1520 1324-1471 1226-1373 1226-1373 1226-1373 1177-1324	1716-1863 1618-1765 1569-1716 1520-1667 1471-1618 1373-1520 1373-1520 1373-1520 1373-1520	1618-1765 1569-1716 1569-1716 1520-1667 1471-1618

C. FORMABILITY

Specification	Torsion Test	Bend Test (180°)	Wrap Test
BS 2803 A229 J316 A230 J351 DIN 17223 FD VD SIS 1770	1.5 to 10 mm - - By agreement 1 mm to 7.5 mm*	> 3 mm - - - -	1 to 3 mm on 1d < 4 mm on 1d > 4 mm to 8 mm on 2d < 4 mm on 1d > 4 mm to 6.5 mm on 2d
G3560	-	> 6 mm**	< 4 mm on 1d > 4 mm on 2d
G3561	2.0 to 6 mm*	-	< 4 mm on 1d > 4 mm on 2d

- * Reverse torsion test
- ** 90° bend angle

Commentary:

The wrap test is the most common method of assessing formabi8lity, the bend test being the least popular. Both Germany and Japan favour a reverse torsion for valve spring quality wires. Only the UK applies all three methods of assessing formability.

D. SURFACE QUALITY

	Total	4% or 0.25 mm 3% or 0.2 mm 1.5% or 0.12 mm 0.5% or 0.01 mm	2% on < 6 mm wire 0.125 mm on) 1 3 1 3 1 3 1 3 1	ı	1.5% or 0.05 mm
Decarburisation	Gradient	rem rem 0.5% or 0.01 mm	ı	1		Statement
Decarbu	Partial	1% or 0.06 mm 0.75% or 0.05 mm 0.375% or 0.03 mm Nil	< 0.04 mm	0.025 mm on < 4.8 mm wire 0.0375 mm on > 4.8 mm wire		General
	Complete	0.8% or 0.05 mm Nil Nil	Ni1 0.5%	N±1	Nil	Lin
Max Defect Depth		3% or 0.2 mm 2% or 0.15 mm 1% or 0.1 mm Nil	General statement 3.5% or 0.25 mm	General statement	General statement General statement	General statement 0.01 mm < 2 mm wire 0.5% on > 2 mm wire
Deep Etch Test		All sizes All sizes All sizes All sizes	All sizes -	All sizes	- All sizes	All sizes All sizes
Specification		BS 2803 NS HS ND HD	A230 J316	1351	DIN 17223 FD VD	SIS 14-17-70 63560 63561

N.B. The defect and decarburisation levels specified are qualified, "whichever is the smaller"

Commentary:

Within the British standard there are four quality grades compared with two in the German standard. The remaining standards only define one quality. Foreign standards for general purpose spring wire tend to specify quality only in the broadest terms — if at all! More specific information is provided for the high quality valve spring wires but this is not as comprehensive as that given for the British ND and HD qualities.

Materials having broadly similar compositions which could be used as prehardened and tempered spring steel wire include the following:-

UK - En 42

US - SAE/AISI 1060, 1070, 1078

Germany - WkSt 1.1230, 1.1250, 1.1231, Ck67

France - XC65, XC70

Italy - C70

5. 1% CHROME-VANADIUM OIL HARDENED AND TEMPERED SPRING WIRE

A. COMPOSITION

Wire Specification	Origin	Steel Grade	%C min max	% Si min max	% Mn min max	s s max	% P min max	% Cr min max	% V min
BS 2803 1980	눔	735A50	.46 .54	.10 .35	06. 09.	.035	.035	.80 1.10	0.15
ASTM A231:83	SN		.48 .53	.15 .35	.70 .90	.040	.040	.80 1.10	0.15
ASTM A232:77	Sn		.48 .53	.20 .35	.70 .90	.035	.020	.80 1.10	0.15
SAE J132 1974	SN		.48 .53	.20 .35	.70 .90	.035	•020	.80 1.10	0.15
SIS 14-22 30	MS	22 30	.48 .55	.15 .40	.70 1.00	.035	.035	.90 1.20	0.10 - 0.2
JIS 63565:86	Japan	SWDCV-V	.45 .55	.15 .35	.65 .95	.025	.025	.80 1.10	.1525

B. TENSILE STRENGTH

			Strength F	R _m (N/mm ²)		
Wire Diameter	BS 2803	A231	A232	J132	14-22-30	G3565
0.5		2060-2260	2070-2240	2070-2240		
1.0	1970-2120	1940-2100	1930-2100	1930-2100		
2.0	1780-1930	1780-1930	1760-1900	1760-1900	1600-1800	1570-1720
3.0	1670-1820	1660-1800	1640-1780	1640-1780	1550-1750	1570-1720
4.0	1580-1730	1580-1720	1565-1700	1565-1700	1500-1700	1520-1670
5.0	1530-1680	1520-1640	1500-1640	1500-1640	1450-1600	1470-1620
6.0	1490-1640	1460-1600	1460-1600	1460-1600	1400-1550	1470-1620
7.0	1450-1600	1420-1560	1430-1565	1430-1565	1350-1500	1420-1570
8.0	1430-1580	1400-1540	1400-1540	1400-1540	1350-1500	1370-1520
9.0	1400-1550	1380-1520	1380-1520	1380-1520	1300-1450	1370-1520
10.0	1380-1530	1360-1500	1360-1500	1360-1500	1300-1450	1370-1520
12.5	1360-1510	1320-1460	1320-1455	1320-1455	1250-1400	

Note:- Specifications A231, A232, J132 and G3565 specify minimum reduction of area values on wires above 2.0mm diameter, e.g. 45% minimum R of A up to but not including 4.0mm. Above 4mm a 40% minimum is stipulated.

C. FORMABILITY

Specification	Torsion Test	Bend Test (180 ⁰)	Wrap Test
BS 2803	1.5 to 10 mm	>3 mm	1 to 3mm on 1d
A 231	-	_	<4mm on 1d 4 to 8mm on 2d
A 232	-	-	<4mm on 1d 4 to 8mm on 2d
J 132	-	-	<4mm on 1d 4 to 8mm on 2d
14-22-30	-	>4 mm	up to 4mm on 2d
G 3565	<6 mm	>6 mm*	<4mm on 1d >4mm on 2d

* 90° bend angle

D. SURFACE QUALITY

				Decarburisati	lon	
Specification	Deep etch Test	Max. Defect Depth	Complete	Partial	Gradient	Total
BS 2803 HS	All sizes	2% or 0.15mm	NIL	.75% or .05mm	rem	3% or 2mm
ND	28 24	1% or 0.10mm	NIL	.375% or .03mm	rem	1.5% or .12mm
HD	89 39	NIL	NIL	NIL	0.5% or 0.01mm	0.5% or .01mm
A231	tt ar	3.5% or 0.25mm	<u>-</u>	-	-	-
A232	ss 11	NIL	NIL	.025mm up to 4.88mm .038 above 4.88mm		
J132	19 19	NIL	NIL	(as A232)		
14-22-30	-	Free from harmful defects	_	-	444	-
G3565	11 11	.01mm up to 2mm 0.5% for 2 to 6mm 0.7% or .06mm for wire above 6mm	NIL			1.5% or 0.05mm max

N.B. The defect and decarburisation levels specified are qualified, "whichever is the smaller".

Commentary:

The German standards authority (DIN) does not publish a specification for oil hardened and tempered 1% CrV spring wire. Materials having broadly similar compositions which can be classed as such include the following steel grades:

Germany - 50 CrV4, Wk.St. 1.8159

UK - 735A50, En 47

US - SAE/AISI 6150

France - 50 CV4

Japan - SUP10, SWOCV-V

Sweden - 22-30

6. SILICON-CHROME PRE-HARDENED AND TEMPERED SPRING WIRE

A. COMPOSITION

Wire Specification	Origin	Steel Grade	min	C max	%S: min	i max	% min	ln max	%S max	%P max	%C min	r max
BS2803 1980	UK	685A55	0.5	0.6	1.2	1.6	0.5	0.8	0.025	0.03	0.5	0.8
ASTM A401:77	US		0.51	0.59	1.2	1.6	0.6	0.8	0.04	0.035	0.6	0.8
SAE J157:70	US		0.51	0.59	1.2	1.6	0.6	0.8	0.04	0.035	0.6	0.8
JIS G3566:86	Japan	SWOSC-V	0.5	0.6	1.2	1.6	0.5	0.8	0.025	0.025	0.5	0.8

Commentary:

The chemical composition of the above four specifications are, for all practical purposes, the same, but attention is drawn to the slight differences in the sulphur and phosphorus contents between the specifications. With modern steel making practice, it is unlikely that the maximum levels quoted for the U.S. standards will be achieved.

B. TENSILE STRENGTH

Wire		Str	ength Rm (N/mm	²)	
Dia (mm)	BS2803 Range 1	BS2803 Range 2	A401	J157	G3566
0.5 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0	1950-2100 1830-1980 1750-1900 1680-1830 1630-1780 1590-1740 1560-1710 2540-1690 1520-1670 1500-1650 1460-1610	2100-2250 1980-2130 1900-2050 1830-1980 1780-1930 1740-1890 1710-1860 1690-1840 1670-1820 1650-1800 1610-1760	2050-2230 1970-2140 1880-2050 1820-1990 1770-1940 1740-1910 1710-1880 1690-1850 1660-1830 1640-1810	2050-2230 1970-2140 1880-2050 1820-1990 1770-1940 1740-1910 1710-1880 1690-1850 166011830 1640-1810	1910-2060 1860-2010 1810-1960 1760-1910 1710-1860 1660-1810 1660-1810

Note: Specifications A401, J157 and G3566 specify minimum reduction of area values, e.g. A401 and J157 - 2.3mm to 3.4mm, 45% R of A min, > 3.4mm, 40% R of A min. G3566 - 3.5mm and smaller, 45% R of A min, > 3.5mm, 40% R of A min.

Commentary:

The UK is the only major country having two tensile ranges for siliconchrome spring wire. The two American specifications have identical tensile strengths and are very similar to those for the Range 2 British material. The tensile strengths for Japanese wires are somewhat lower.

C. FORMABILITY

Specification	Torsion Test	Bend Test (180 ⁰)	Wrap Test
BS2803	1.5 to 10mm	>3mm	1mm to 3mm on 1d
A401		· 	<4mm on 1d
J157			4 to 8mm on 2d <4mm on 1d
G3566	<6mm	>6mm*	4 to 8mm on 2d <4mm on 1d >4mm on 2d

* 90° bend angle

Commentary:

The only test which is common to the four specifications is the wrap test. There is no requirement for a torsion or bend test in the American standards.

D. SURFACE QUALITY

					Decarbur	isation	
Specifica	Specification Deep Etch test		Max defect depth	Complete	Partial	Gradient	Total
BS2803	HS	all sizes	2% or 0.15mm	Nil	.75% or .05mm	rem	3% or .2mm
	ND	11 19	1% or 0.1mm	\Nil	.375% or .03mm	rem	1.5% or .12mm
	HD	n n	Nil	Nil	Nil	0.5% or 0.01mm	0.5% or .01mm
A401		n "	3.5% or .25mm				
J157			3.5% or .25mm	0.5% max	1.5% max		2% max
G3566		all sizes	.01% upto 2mm, .5% for 2 - 6mm, .7% for over 6mm	Nil			1.5% or 0.05mm

NB The defect and decarburisation levels specified are qualified "whichever is the smaller".

Commentary:

It should be noted that the British standard specifies three quality grades, whereas the foreign stardards define only one. The allowable maximum defect and decarburisation levels in American specifications are more generous than those for wire produced to Japanese or British standards.

Materials having broadly similar compositions which can be classed as siliconchrome spring steels include the following:-

UK - 685A55, En 48A

US - SAE/AISI 9254

Germany - 67SiCr5, Wk.St. 1.7103

France - 60SC7

Japan - SWOSC-V, SUP12

The German (DIN) and the Swedish (SIS) standards authorities do not publish specifications for oil hardened and tempered silicon-chrome spring wire.

7. STAINLESS STEEL SPRING WIRE

Stainless steel spring materials develop their high strength by cold working. Although essentially austenitic, these materials can become weakly magnetic due to the transformation of austenitic to a martensite-type structure as a result of the cold drawing process. This transformation is dependent on the actual composition of the material and, where applications demand "non-magnetic" stainless steel springs, care is required in selecting a suitable material composition which will remain austenitic on cold drawing.

This section is devoted to straight 18-8 type stainless steels.

A. COMPOSITION

Wire Specification	Origin	Steel Grade	%C Max	%Si Max	%Mn Max	%S Max	%P Max	%Cr	%Ni	%N Max
BS2056 1983	UK	302s26	0.12	1.0	2.0	0.03	0.045	17-19	7.5-10.0	
S205	UK	_	0.15	0.2-1.0	0.5-2.0	0.025	0.035	17-19	7.5-9.0	
1969 ASTM,A313	ບຣ	302	0.15	1.0	2.0	0.03	0.045	17-19	8-10.0	0.1
1981		304 305	0.08	1.0	2.0	0.03	0.045 0.045	18-20 17-19	8-10.5 10.5-13.0	0.1
SAE,J230 1971	US	30302	0.15	1.0	2.0	0.03	0.045	17-19	8.0-10.0	
DIN 17224 1982	Germany	1.4310	0.12	1.5	2.0	0.03	0.045	16-18	6.0-9.0	
SIS 14-23-31 1972	Sweden	2331-06	0.12	1.0	2.0	0.03	0.045	17-19	7.0-9.5	
J.I.S G4314 1984	Japan	sus302 " 304	0.15 0.08	1.0	2.0	0.03	0.045	17-19 18-20	8.0-10.0 8.0-10.5	
		" 304NI	0.08	1.0	2.5	0.03	0.045	18-20	7.0-10.5	0.1-0.2

Commentary:

In general, European standards contain only one grade of straight 18-8 type stainless steel whereas the American and Japanese include three. Unlike the European standards, the US and Japan offer nitrogen-stabilised material. Compared with other compositions under review, the German wires tend to be somewhat lower in Cr and Ni which will promote more rapid work hardening on cold drawing, along with a greater likelihood of the wire becoming 'magnetic'.

B. TENSILE STRENGTH

	Strength Rm (N/mm²)									
Wire Dia (mm)	BS 2056 :	302s26 G2	s205	A3 302 & 304	305	J230 30302	DIN 17224 1.4310	SIS 14-23-31 23 31-06	JI: Class A (WPA) SUS 302, 304,304NI	S G4314 Class B (WPB) SUS 302, 304,304NI
0.10 0.25 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0	1880-2160 1880-2060 1720-1960 1620-1860 1430-1670 1230-1470	2160-2400 2060-2300 1960-2200 1860-2100 1670-1910 1470-1710 1370-1610 1370-1610 1280-1520 1280-1520 1230-1470	2150 min 2050 min 1850-2050 1650-1850 1550-1750 1400-1600 1300-1500 1200-1400 1100-1300 1000-1200 1000-1200	2240-2450 2205-2415 2070-2275 1895-2095 1695-1895 1530-1745 1415-1620 1295-1515 1205-1415 1160-1365 1070-1280 1035-1240 1000-1205 930-1150	1690-1895 1690-1895 1620-1825 1620-1825 1450-1655 1345-1550 1240-1450 1105-1310 1035-1240 965-1170 930-1140 895-1105	2240-2450 2205-2415 2070-2275 1850-2070 1695-1895 1530-1745 1415-1620 1280-1475 1205-1415 1110-1325 965-1170	2200-2450 2100-2350 2000-2250 1900-2150 1700-1950 1500-1750 1400-1650 1400-1650 1300-1550 1300-1550 1250-1500	2110 min 2010 min 1960 min 1760 min 1670 min 1570 min 1470 min 1470 min 1270 min 1270 min	1618-1863 1569-1814 1569-1814 1471-1716 1324-1569 1177-1422 1177-1422 1079-1324 1079-1324 981-1226 981-1226	2157-2403 2059-2305 1961-2206 1863-2108 1667-1912 1471-1716 1471-1716 1373-1618 1373-1618 1275-1520 1275-1520 1128-1373 981-1226 883-1128

Note: - DIN 17224 stipulates a minimum of 40% R of A for wires over 1.5mm.

Commentary:

The national standard having the highest tensile strength over the complete size range is the German DIN 17224, which could be attributed to the leaner alloy content. The tensile strengths of the British Grade 2, the Swedish and the Japanese Class B wires are very similar.

Both Japan (Class A wire) and the USA (305 wire) recognise the need for spring wires of lower tensile strength where increased formability would aid spring manufacture.

C. FORMABILITY

Specification	Torsion Test	Bend Test (180 ⁰)	Wrap Test	Reverse Bend Test	Wrap and Stretch Test
BS2056:302S26	——————————————————————————————————————	>3mm on 2d >6mm on 3d	<3mm on 1d	es and and a second	
s205	<2mm		<3mm	>3mm	·
A313:302,304 and 305	, 	, 	<4mm on 1d >4mm on 2d	>0.6mm	<4.5mm
J230		<u></u>	<4mm on 1d > 4mm on 2d		<2.5mm
DIN 17224	>1.5mm	<u></u>			<1.5mm
SIS 14-23-31			<4mm		
G4314	<4.Omm				· · · · · · · · · · · · · · · · · · ·

Commentary:

The torsion test is used only to reveal surface defects and not as a measure of formability. The most common test for formability is the wrap test and is used in all standards except the Japanese specification. The United Kingdom is the only country specifying a bend test for stainless steel wires not surprising considering the practical difficulties in undertaking such a test on a routine basis.

D. SURFACE QUALITY

Specification	Deep Etch Test	Max. Defect Depth (mm)
BS2056:302S26 S205 A313 J230 DIN 17224 SIS 14-23-31 G4314	all sizes	(note 1) (note 2) ————————————————————————————————————

Note 1:- No quantitative data is given, only general statements to the effect that the material should be free from harmful defects.

Note 2:- Visual examination after torsion testing but again no quantitative defect levels quoted.

Commentary:

The loss of carbon at the surface of stainless steel wires has no significant effect on the properties and therefore no decarburisation requirement is specified. On the other hand, stainless wires are probably more prone to surface defects than conventional carbon and low alloy spring steel wires, yet none of the standards has attempted to quantify an acceptable surface defect level.

Stainless steel wires having broadly similar compositions include the following:

UK - 302S26, 302S25, En 58A, S205

US - S302, S304, S305, 30302

Germany - Wk.St. 1.4300, 1.4310, X12CrNi 177, X12CrNi188

Sweden - 14-23-31, 14-23-33

Japan - SUS 301, 302, 304

France - Z6CN18.09, Z10CN18.09

8. MOLYBDENUM-BEARING STATNLESS STEEL SPRING WIRE

Stainless steels containing molybdenum are similar in many respects to the 'austenitic' 18/8 type stainless steels, although the additional molybdenum somewhat improves their corrosion resistance. The addition of 2 to 3% molybdenum to the straight 18/8 variety of stainless enhances corrosion resistance under most conditions but especially where exposure to sulphuric acid, organic acids, halogen salts and sea water is encountered.

A. COMPOSITION

Wire Specification	Origin	Steel Grade	%C Max	%Si Max	%Mn Max	%S Max	%P Max	%Cr	%Ni	% M O
BS2056 1983	UK	316542	0.07	1.0	2.0	0.03	0.045	16.0- 18.5	9.5- 13.5	2.0- 2.5
ASTM, A313 1981	ບຣ	316	0.08	1.0	2.0	0.03	0.045	16.0- 18.0	10.0- 14.0	2.0- 3.0
DIN 17224 1982	Germany	1.4401	0.07	1.0	2.0	0.03	0.045	16.5- 18.5	10.5- 13.5	2.0- 2.5
SIS 14 23 47 1985	Sweden	47-04	0.07	1.0	2.0	0.03	0.045	16.0- 18.5	10.5- 14.0	2.0- 2.5
JIS G4314 1984	Japan	sus 316	0.08	1.0	2.0	0.03	0.045	16.0- 18.0	10.0 14.0	2.0- 3.0

Note:- The German steel grade 1.4401 is also designated as X5 Cr Ni Mo 1810.

Commentary:

All steel compositions are very similar, with the British standard having the leanest alloy content. The United States and Japanese steel compositions are identical, allowing higher percentages of molybdenum than their European counterparts.

B. TENSILE STRENGTH

	Strength R _m (N/mm ²)						
Wire Dia (mm)	BS2056 316S42	A313 316	DIN 17224 1.4401	SIS 14 23 47 23 47-04	G 4314 SUS316		
0.10 0.25 0.50 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0	1680-1920 1640-1880 1600-1840 1580-1820 1460-1700 1260-1500 1100-1340 1100-1340 1030-1270 1030-1270 860-1100 860-1100	1690-1895 1690-1895 1620-1825 1620-1825 1450-1655 1345-1550 1240-1450 1105-1310 1035-1240 965-1170 930-1140 895-1105 895-1105	1650-1900 1600-1850 1600-1850 1500-1750 1350-1600 1200-1400 1100-1350 1100-1350 1050-1300	1700 min 1650 min 1600 min 1500 min 1400 min 1350 min 1200 min 1200 min 1100 min 1100 min	1618-1863 1569-1814 1569-1814 1471-1716 1324-1569 1177-1422 1177-1422 1079-1324 1079-1324 981-1226 981-1226		

<u>Note</u>:- DIN 17224 specifies a minimum of 40% reduction of area on tensile testing for wires over 1.5mm diameter.

Commentary:

There does not appear to be any consistent pattern within the strength values quoted to suggest one national specification is significantly higher than another. From a practical stand-point the differences between the various standards are insignificant.

C. FORMABILITY

Specification	Torsion Test	Bend Test (180°)	Wrap Test	Reverse Bend Test	Wrap and Stretch Test
BS2056:316S42		>3mm on 2d >6mm on 3d	<3mm on 1d		
A313:316			<pre><4mm on 1d >4mm on 2d</pre>	>0.6mm	<4.5mm
DIN 17224:1.4401	>1.5mm				<1.5mm
SIS 14 23 47-04			<4mm		
G4314:SUS316	<4mm			-	

Commentary:

The formability requirements given for molybdenum-bearing stainless steels are precisely the same as those given for straight 18/8 type stainless steel wires. The wrap test is the most popular method of assessing formability of wire. Where a torsion test is specified, it is not used to gauge formability but rather to reveal surface imperfections in the material.

D. SURFACE QUALITY

Specification	Deep Etch Test	Max Defect Depth (mm)
BS2056:316S42		(note 1)
A313:316		
DIN 17224:1.4401		(note 2)
SIS 14 23 47-04		(note 1)
G4314:SUS316		(note 2)

Note 1: Only general statements are given in the standards to the effect that wires should be free from harmful defects.

Note 2: Visual examination is required after torsion testing but no quantitative defect levels are given.

Commentary:

In view of the fact that stainless steel wires are more prone to surface imperfections than carbon steels, it is surprising that none of the standards includes a deep etch test to reveal defects, nor specifies acceptable levels of defects.

In addition to the steels considered in this comparison, there are a number of other materials having broadly similar compositions:

UK - 315S16 (En 58H), 316S16 (En 58J)

US - Wk.St. 1.4404 (X2CrNiMo1810), 1.4410 (G-X10CrNiMo18), 1.4408 (G-X6CrNiMo1810)

Sweden - 14 23 48, 14 23 43, 14 23 53

Japan - SUS 32TB, SUS 316L

France - AFNOR Z6CND17.11, Z2CND17.12

9. 17/7 PH STAINLESS STEEL SPRING WIRE

Precipitation hardening 17/7PH stainless steel wire is strengthened by a combination of cold working and thermal treatment after spring coiling. The material possesses good corrosion resistance and is particularly useful where high working stresses are encountered.

A. COMPOSITION

Wire Specification	Origin	Steel Grade	%C max	%Si max	%Mn max	%S max	%P max	%Cr	₹Ni	%Al
BS2056 1983	UK	301891	0.09	1.0	1.0	0.03	0.045	16-18	6.5-7.75	0.75-1.50
DTD 5086 1969	UK		0.09	1.0	1.0	0.025	0.035	16-18	6.5-7.75	0.75-1.50
ASTM A313:81	ບຣ	631	0.09	1.0	1.0	0.03	0.04	16-18	6.5-7.75	0.75-1.50
SAE J217: 70	us		0.09	1.0	1.0	0.03	0.04	16-18	6.5-7.75	0.75-1.50
AMS 5678A:81	us		0.09	1.0	1.0	0.03	0.04	16-18	6.5-7.75	0.75-1.50
DIN 17224:82	Germany	1.4568	0.09	1.0	1.0	0.03	0.045	16-18	6.5-7.75	0.75-1.50
G.4314 1984	Japan	sus 631J1	0.09	1.0	1.0	0.03	0.04	16-18	7.0-8.5	0.75-1.50

Commentary:

All compositions are very similar except for the Japanese material in which the nickel content is somewhat higher.

B. TENSILE STRENGTH

BS2056: s drawn	301s81 after HT*	DTD 5 as drawn	086 after HT*	(N/mm ²) A313 type and AMS 5	631, J217	DIN 17224	G4314,
	after HT*	as drawn	after HT*	and AMS 5	670x	1 _	
200 2110					O / OB	:1.4568	SUS 631J1
200 2110				as drawn	after HT*	as drawn*	as drawn*
200 2112				-nominal			
200 2110							1961-2206
380-2110	2230-2530			2035	2310-2515	1950-2200	1912-2157
320-2050	2170-2470	1800-	2150-	2000	2275-2480	1850-2100	1814-2059
770-2000	2120-2420	1750-2050	2150-2450	1895	2205-2415	1800-2050	1765-2010
630-1860	1930-2210	1650-1950	2000-2300	1760	2015-2220	1600-1850	1569-1814
500-1730	1800-2080	1500-1800	1850-2150	1625	1875-2080	1400-1650	1373-1618
160-1690	1760-2040	1350-1700	1700-2000	1560	1765-1970	1400-1650	1373-1618
100-1630	1680-1950	1350-1700	1700-2000	1530	1740-1945	1300-1550	1275-1520
380-1610	1660-1930	1300-1650	1650-1900	1470	1670-1875	1300-1550	1275-1520
350-1580	1600-1870	1250-1550	1550-1850	1470	1670-1875		
330-1560	1530-1800	1250-1550	1550-1850	1425	1620-1825		
270-1500	1470-1740	1250-1550	1550-1850	1425	1620-1825		
270-1500	1470-1740	1250-1550	1550-1850	1425	1620-1825		
				1400	1585-1795		
ł				1400	1585-1795	:	
1		7					
4C 38 35 33	00-1630 00-1610 00-1580 00-1560 00-1500	00-1630	00-1630 1680-1950 1350-1700 00-1610 1660-1930 1300-1650 00-1580 1600-1870 1250-1550 00-1560 1530-1800 1250-1550 00-1500 1470-1740 1250-1550	00-1630 1680-1950 1350-1700 1700-2000 00-1610 1660-1930 1300-1650 1650-1900 00-1580 1600-1870 1250-1550 1550-1850 00-1560 1530-1800 1250-1550 1550-1850 00-1500 1470-1740 1250-1550 1550-1850	10-1630 1680-1950 1350-1700 1700-2000 1530 10-1610 1660-1930 1300-1650 1650-1900 1470 10-1580 1600-1870 1250-1550 1550-1850 1470 10-1500 1470-1740 1250-1550 1550-1850 1425 10-1500 1470-1740 1250-1550 1550-1850 1425 10-1500 1470-1740 1250-1550 1550-1850 1425 1400 1400 1400	1680-1950 1350-1700 1700-2000 1530 1740-1945 160-1610 1660-1930 1300-1650 1650-1900 1470 1670-1875 160-1560 1530-1850 1250-1550 1550-1850 1425 1620-1825	1680-1950

* Details of the precipitation heat treatment are given in each of the standards. The majority specify 480° +/- 10°C for 1 to 2 hours, although the Japanese specify 470° +/- 10°C for 1 hour. For the German & Japanese steels, the as-drawn values are increased by 260-400 and 245 min respectively.

Commentary:

The three standards have identical tensile strengths but the as-drawn tensile strengths show differences from country to country, in excess of 100N/mm² in some cases. The strength values for the German and Japanese wires are generally lower than those quoted in British specifications. Only the DIN standard requires a minimum reduction in area of 40% after tensile testing on wires over 1.5mm diameter.

C. FORMABILITY

Specification	Torsion Test	Bend Test (180 ⁰)	Wrap Test	Reverse Bend Test	Wrap and Stretch Test
BS2056:301S81		>3mm on 2d >6mm on 3d	<3mm on ld		
DTD5086	<2mm		<3mm	>3mm	
A313:type 631			<4.1mm on ld >4.1mm on 2d	_	<4.5mm
J217			all sizes on ld		<3mm
AMS 5678A			all sizes on 1d		<3.1mm
DIN 17224	>1.5mm				<1.5mm
G4314	<4mm				

Commentary:

Although the torsion test is specified in three of the standards it is not primarily intended to measure the ductility of the material but rather as a test to reveal surface defects in the wire. Most standards favour a wrap test as an indication of formability. With two of the foreign standards there is no provision for measuring formability on large diameter wires.

D. SURFACE QUALITY:

Specification	Deep Etch Test	Max Defect Depth
BS2056:301S81		(Note 1)
DTD 5086	all sizes	1.5% or 0.025mm whichever is smaller
A313:type 631	all sizes	(Note 1)
. J217		(Note 1)
AMS 5678A		(Note 1)
DIN 17224		(Note 2)
G4314		(Note 2)

Note 1:- No quantitative information is given, only general statements such as 'free from harmful defects' are specified.

Note 2:- Visual examination after torsion testing but no quantitative values given.

Commentary:

Since the carbon content of stainless steels is very low, there is no requirement for specifying decarburisation levels. It is surprising that only two of the standards stipulate deep etch testing as a means of revealing surface defects.

Materials having broadly similar compositions which are classified as 17/7PH steels include the following:

UK - 301S81, DTD 5086

US - Type 631, J217, AMS 5678A

Germany - Wk.St. 1.4568, X7CrNiAl177

Japan - SUS 631, SUS 631J1

International - ISO 683/XVI Type 2

10. SPRING BRASS AND COPPER-NICKEL SPRING WIRE

Although not as widely used as phosphor-bronze material, spring brasses find application where material costs are a first consideration. They possess excellent electrical conductivity and good all-round corrosion resistance. In certain environmental conditions, such as damp atmospheres containing ammonia, cold drawn brass wires may be sensitive to "season cracking".

Copper-nickel (also known as "Nickel Silver" and "German Silver") is more expensive and is principally used in telecommunications and optical industries. It is silvery-white in colour and has good resistance to corrosion.

Both spring brass and copper-nickel develop their strength from cold working and cannot be hardened by thermal treatments.

A. COMPOSITION

Wire Specification	Origin	Grade	% Cu	% Zn	% Ni	% Mn
BS 2873:1969	U.K.	CZ 107 NS 106	64.0/ 67.0 60.0/ 65.0	Rem. Rem.	17.0/ 19.0	0.05/ 0.5
ASTM B134:86 B206:86	USA	C 27000 C 76400	63.0/ 68.5 58.5/	Rem.	16.5/	
DIN 17682:79	Germany	CuZn36 (2.0335) CuNi18 Zn20	61.5 63.5/ 65.0 60.0/ 63.0	Rem.	19.5 17.0/ 19.0	0.5 max
JIS H3270:86	Japan	(2.0740) C 7521	61.0/ 67.0	Rem.	16.5/ 19.5	0.5 max

Note:- The German DIN standard 17682 does not specify compositions but refers to other standards for this information e.g. CuZn36 - DIN 17660 and CuNi18Zn20 - DIN 17663. The numbers given in parenthesis below the German grades are alternative Werkstoff material designations.

Commentary:

The compositions for the brasses are very similar from country to country.

On the other hand, the USA seems to favour a slightly lower copper content for their copper-nickel alloy. The Japanese do not include a spring brass in their national specifications.

B. TENSILE STRENGTH

Specification	Grade	Condition	Wire diameter (mm)	Tensile Strength (N/mm ²)
			over up to	min max
BS 2873:69	CZ 107	0 1/2 H H EH EH	0.5 10.0 0.5 10.0 0.5 10.0 2.5 2.5 6.0	320 - 460 620 620 740 740 820 700 770
	NS 106	1/2 H H	by agreement	
ASTM B134:86	C27000	H00 H01 H02 H03 H04 H06 H08	12.0 9.5 6.3	345 450 425 530 545 650 635 740 700 810 790 890 830 —
ASTM B206:86	C76400	H01 H02 H04 H08	0.5 0.65 0.65 1.60 1.60 3.0 3.0 6.0	510 640 635 760 770 885 900 - 860 830 830
DIN 17682:79	CuZn36		0.3 0.8 0.8 1.5 1.5 3.0 3.0	750 930 700 850 650 770 by agreement
	CuNil8 Zn20	·	0.3 0.8 0.8 1.5 1.5 3.0 3.0	860 1040 830 980 800 920 by agreement
JIS H3270:86	C7521	0 1/2 H H	0.5 0.5 5.0 0.5 5.0	373 520 520 686 667

Note: The wire condition is also referred to as the temper grade in the Japanese and ASTM standards. It should be noted that the various designations for wire condition/temper grade do not necessarily equate to the same tensile strength from country to country.

In the current ASIM standards for copper-based alloys, a new series of temper designations has been introduced and these equate to the old designations as given below:-

New temper grades	Old temper grades
061 H00 H01 H02 H03 H04 H06 H08 H10	Annealed Eighth—hard Quarter—hard Half—hard Three—quarter—hard Hard Extra—hard Spring—hard Extra—spring hard

C FORMABILITY

Specification	Grade	Wrap test condition size		Bend Test condition size		Tensile Property condition %El(min	
BS 2873:69	CZ107	н, ен	<6mm			0	35%
ASTM B206	C76400			но8	<6.5mm	н08	5-9% (depending on size)
DIN 17682	CuZn 36	all	<1.5	all	all		
	CuNil8 Zn20	all	<1.5 mm	all	all		

Commentary:

The British and German standards favour a wrap test for assessing formability but this is often limited to smaller wire sizes. There appears to be little consistency between the various national standards regarding formability testing in that the UK has no requirements placed on the coppernickel alloy nor the USA on formability of spring brass.

The DIN standard specifies a modified wrap test which involves stretching the helix after wrapping.

D. SURFACE QUALITY

Only DIN 17682 makes reference to the required surface quality of the wires and stipulates that defects and scores should be limited to a maximum of 1% of the wire diameter and not more than 0.006mm. The British and Japanese standards make only general statements that wires shall be free from harmful defects without any further qualification.

None of the American ASTM specifications makes any reference to surface quality.

11 PHOSPHOR BRONZE SPRING WIRE

Copper-based spring wires represent a group of materials which, due to their good electrical conductivity and appreciable resistance to corrosion, find wide application in electrical equipment. Almost invariably these materials develop their mechanical strength from cold working by drawing. They do not, however, develop the strength values attainable with ferrous materials and this feature must be recognised when designing springs from copper based materials.

Phosphor-Bronze wires are the most widely used of the copper-based alloys.

A. COMPOSITION

Wire Specification	Origin	Grade	% Cu	% Sn	% P
BS 2873:1969	U.K.	PB 102 PB 103	Rem. Rem.	4.5/6.0 6.0/7.5	0.02/0.40 0.02/0.40
ASTM B 159:86	USA	C51000 C52100	Rem. Rem.	4.2/5.8 7.0/9.0	0.03/0.35 0.03/0.35
DIN 17682:79	Germany	Cu Sn 6 (2.1020) Cu Sn 8 (2.1030)	Rem.	5.5/7.0 7.5/8.5	0.01/0.35
JIS H3270:86	Japan	C5102 C5191	Rem. Rem.	4.5/5.5 5.5/7.0	0.03/0.35 0.03/0.35

Note:- The DIN standard 17682 does not specify compositions but refers to another standard for this information - DIN 17662. The numbers in parenthesis immediately below the German grade designations refer to the corresponding Werkstoff material numbers.

<u>Commentary</u>: In general the compositions of the various grades of phosphor bronze are very similar.

B. TENSILE STRENGTH

Specification	Grade	Condition		oiameter	Tensile Strength R
			over	up to	min max
BS 2873	PB 102	0 1/2H H EH EH	0.5 0.5 0.5	10.0 10.0 10.0 2.5 6.0	340 – 540 700 700 850 850 –
	PB 103	0 1/2H H EH EH	0.5 0.5 0.5 2.5	10.0 10.0 10.0 2.5 6.0	800 - 370 - 590 740 740 900 900 - 850 -
ASTM B159:86	C51000	061 H01 H02 H03 H04 H08	0.6 1.6 3.0 6.0 10	14.0 14.0 14.0 14.0 0.6 1.6 3.0 6.0 10.0 16.0	295 400 415 525 550 670 660 795 745 880 1000 930 890 850 830 720
	C52100	061 H01 H02 H03 H04	10	6.0 6.0 6.0 6.0 6.0	365 470 510 625 655 795 780 930 860 1035
DIN 17682:79	Cu Sn 6 and Cu Sn 8		0.1 0.3 0.8 1.5 3.0	0.3 0.8 1.5 3.0	1050 1230 1000 1180 950 1100 900 1020 by agreement
JIS H3270:86	C5102 C5191	0 H 0 1/2H H	0.5 0.5 0.5 0.5 0.5	5.0 - 5.0 5.0	304 422 637 314 461 637 785 834

Note:- The wire condition is also referred to as the temper grade in the Japanese and ASIM standards. It should be noted that the various designations for wire condition/temper grade do not necessarily equate to the same tensile strength from country to country.

In the current ASTM standards for copper-based alloys, a new series of temper designations has been introduced and these equate to the old designations as given below:-

New temper grades	Old temper grades
061 H00 H01	Annealed Eighth—hard Quarter—hard
HO2 HO3 HO4 HO6 HO8	Half—hard Three—quarter—hard Hard Extra—hard Spring—hard
H10	Extra—spring hard

C. FORMABILITY

Specn.	Grade	Wrap condtn	Test Size	Bend condtn	Test size	Tensil condtn	e Property elongatn
BS 2873	PB 102 PB 103	Н, ЕН Н, ЕН	<6mm <6mm			0	40% on 100mm 50% on 100mm
ASTM B 159	C51000			н08	<6.5mm	н08	5 to 9% on 50mm depend- ing on size
DIN 17682	CuSn6&8	all	<1.5mm	all	all		
JIS H3270	C5102 C5191	н 1/2н, н	<1.5mm <1.5mm				

Commentary:

Most standards favour a wrap test as a means of assessing formability but this is often limited to the smaller wire sizes. As with other DIN standards, the Germans specify a modified wrap test which involves stretching the coiled helix after forming.

D. SURFACE QUALITY

Only DIN 17682 makes reference to the required surface quality of the wires and stipulates defects and scores should be limited to a maximum of 1% of the wire diameter and not more than 0.006mm. The British and Japanese standards make only general statements that wires shall be free from harmful defects, without any further qualification.

The American ASTM specification makes no reference to surface quality.

12 COPPER BERYLLIUM SPRING WIRE

Within the group of copper-based alloys, copper beryllium has the highest strength derived from its ability to be hardened by cold working followed by a simple thermal treatment. Its use is recommended where the working stresses encountered in service could not be tolerated by other copper-based alloys. Although much more expensive than the other materials in this group, copper beryllium wire finds wide application in instruments and electrical components.

A. COMPOSITION

Wire Specification	Origin	Grade	% Cu	% Be	% Ni+Co	% Co
BS 2873:1969 ASTM: B197:85	UK	CB 101	Rem Rem	1.70/ 1.90 1.80/	0.05/ 0.40 0.2min	
DIN 17682:79	Germany	CuBe2 (2.1247)	Rem	2.0 1.80/ 2.10	0.2.11.11	
		CuCoBe (2.1285)	Rem	0.4/		2.0/
JIS H3270:86	Japan	C1720	Rem	1.80/	0.2min	

Note:- The DIN standard 17682 does not specify compositions but refers to another standard for this information, viz:- CuBe2 and CuCoBe - DIN 17666. The numbers in parenthesis immediately below the German grade designations refer to the corresponding Werkstoff material numbers.

Commentary:

In general the compositions of the various grades are very similar but the Germans include a low beryllium variety which contains a significant amount of cobalt. However, this low beryllium alloy is not capable of achieving the same high tensile strength as the standard 2% Be alloy.

B TENSILE STRENGTH

Specification	Grade	Condition	(Diameter nm) up to, incl	Tensi R _m min	le Stren (N/mm ² max	gth)
BS 2873:69	CB 101	W W(H) WP W(H)P	0.5	10.0 3.0 10.0 3.0	390 770 1050 1240	- - -	
ASTM B197:85 DIN 17682:79	C17200	TB00 TF00 TD01 TH01 TD02 TH02 TD03 TH03 TD04 TD04 F42 F120	0.1	2.0 2.0 2.0 2.0 3.0	400 1105 620 1205 760 1275 895 1310 965 1345 420 1200	540 1310 795 1415 930 1480 1070 1585 1140 1585 550 1300	after h.t. after h.t. after h.t after h.t after h.t after h.t after h.t as drawn after h.t
	CuCoBe	F65 F125 F80 F135 F95 F140 F25 F65 F50 F75 F60 F80	0.1	3.0	650 1250 800 1350 950 1400 250 650 500 750 600 800	800 1400 950 1450 1150 1550 370 800 650 900 750 1000	as drawn after h.t as drawn after h.t
JIS H3270:86	C1720	0 1/4H 3/4H	0.5 0.5 0.5 0.5 0.5	5.0 5.0 5.0 5.0	392 1098 618 1206 834 1304	539 1324 804 1422 1069 1589	annealed after h.t. drawn after h.t. drawn after h.t.

Note:- The wire condition is also referred to as the temper grade in the Japanese and ASTM standards. It should be noted that the various designations for wire condition/temper grade do not necessarily equate to the same tensile strength from country to country.

In the current ASTM standard for copper beryllium alloys, a new series of temper designations has been introduced which equate to the old designations as given over:~

New temper grades	Old temper grades
mnoo.	1 1 (1)
TBOO	Annealed (A)
TDO1	Quarter-hard (1/4H)
TDO2	Half-hard (1/2H)
TDO3	Three-quarter-hard (3/4H)
TDO4	Hard (H)
TFOO	Annealed then pptn hardened (AT)
THO1	1/4 hard " " (1/4HT)
THO2	1/2 hard " " (1/2HT)
THO3	3/4 " " " (3/4HT)
THO4	Hard " " (HT)

C. FORMABILITY

Specification	Grade	Wrap Test Condition size		Bend Test Condition siz	
BS2873	CB101	W(H)	<1.5mm		
ASTM B 197	C17200	all tempers,	all sizes		
DIN 17682	CuBe 2 CuCoBe	all all	<1.5mm <1.5mm	all all	all all

Commentary:

The standards favour a wrap test as a means of assessing formability but often only for the smaller wire sizes. As with other DIN standards, the Germans specify a modified wrap test which involves stretching the coiled helix after forming. It should be noted the Japanese standard has no tests specified for assessing formability.

D. SURFACE QUALITY

Only DIN 17682 makes reference to the required surface quality of the wires and stipulates that defects and scores should be limited to a maximum of 1% of the wire diameter and not more than 0.006mm. The British and Japanese standards make only general statements that wires shall be free from harmful defects without any further qualification.

The American ASTM specification makes no reference to surface quality.